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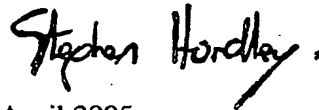
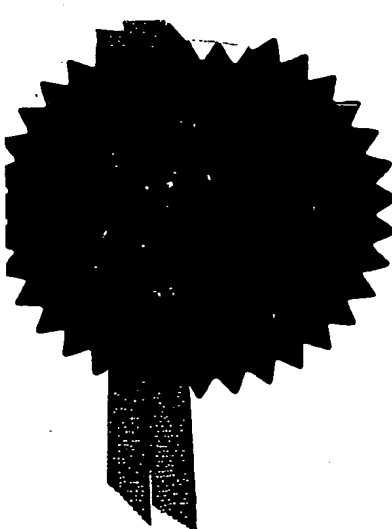
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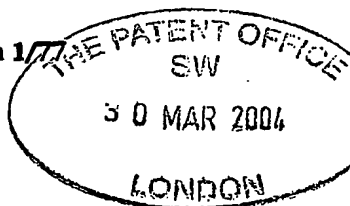
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Remtons Limited,
5 Crosfields Close,
Reading,
Berkshire RG2 9AY,
United Kingdom

Patents ADP number (if you know it)

If the applicant is a corporate body, give the country/state of its incorporation

8793291001

4. Title of the invention

SCANNING APPARATUS

5. Name of your agent (if you have one)

Forrester Ketley & Co.

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

Forrester House
52 Bounds Green Road
London
N11 2EY

Patents ADP number (if you know it)

133001

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Patents Form 1/77

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Continuation sheets of this form

Description 17 —

Claim(s) 5 —

Abstract

Drawing(s) 7 *1 7 8*

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Priority documents

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Statement of inventorship and right to grant of a patent (Patents Form 7/77)

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11. I/We request the grant of a patent on the basis of this application.

Signature(s) *Forrester Ketley & Co.*

Date 29th March 2004

12. Name, daytime telephone number and e-mail address, if any, of person to contact in the United Kingdom

(020) 8889 6622

fk london@forresters.co.uk

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Title: "Scanning Apparatus"

THE PRESENT INVENTION relates to a scanning apparatus operable in the
5 infrared, sub mm-wave, mm-wave or microwave ranges of electromagnetic
radiation. It is an object of the present invention to provide an improved
scanning apparatus operable with radiation of the wavelengths indicated,
having a large effective aperture and which is able to repeatedly scan, at a high
rate, a two-dimensional (e.g. altitude and azimuth) field of view, and which yet
10 can be constructed at reasonably low expense.

In infra-red imaging systems, use is frequently made of flapping mirrors and
rotary polygons with reflective surfaces to scan the scene. In these infra red
systems the pupil in the scanner is typically 10mm in diameter. In mm-wave or
15 microwave systems however the apertures to be scanned are frequently 1m or
larger in diameter and the use of large flapping mirrors at high scan rates (e.g.
such as to provide ten field scans or "frames" per second or more) is not
practical in these systems. It is known that tilted rotary disks may be used to
scan large apertures but these produce a conical scan pattern or a linear scan
20 with a large amount of pupil wander.

In accordance with a first aspect of the present invention, there is provided
scanning apparatus operable in the microwave, mm-wave and infrared ranges
and comprising a support structure, a primary drum which is mounted in said
25 support structure for rotation relative to the support structure about a central
axis of the primary drum, said primary drum being hollow and internally of
regular polygonal form to provide a number of sides or facets, (ideally, but not
necessarily, an even number of sides or facets), each adapted to transmit such
radiation which is plane polarised in a first direction at 45° with respect to the

rotary axis of the drum and to reflect radiation which is plane polarised in a direction at 45° to the rotary axis of the drum and perpendicular to the said first polarisation direction, such radiation emanating from a field of view of the apparatus, being a field of view which is fixed with respect to said supporting structure, (as opposed to rotating with the primary drum), the arrangement being such that radiation passing into the drum through whichever said side of the drum is currently facing said field of view and passing towards the diametrically opposite side will be plane polarised with a polarisation direction such as to be reflected back by said diametrically opposite side towards the rotary axis of the drum, each said polygon side being configured so as to act, when reflecting such radiation striking that side from within the drum, as a concave mirror, to focus the radiation towards a receiver assembly which includes a radiation detector for such radiation.

In accordance with a second aspect of the invention there is provided scanning apparatus operable in the microwave, mm-wave and infrared ranges and comprising a support structure, a first reflective disc or mirror which is mounted in said support structure for rotation relative to the support structure about a first axis, a second reflective disc or mirror which is mounted in said support structure for rotation relative to the support structure about a second axis, the arrangement being such that radiation from a scene being scanned can reach a reflective surface of the first disc or mirror to be reflected thereby onto a reflective surface of the second disc or mirror, to be reflected by the latter, in turn, onto a further part of the apparatus incorporating a receiver or receivers for such radiation, and wherein said reflective surface of the first disc or mirror has an axis of rotational symmetry, (or a normal where said surface is planar), tilted at a small angle relative to said first axis and wherein said reflective surface of the second disc or mirror has an axis of rotational symmetry (or a normal where said surface is planar) tilted at a small angle relative to said

second axis, and driving means for said discs or mirrors arranged to drive these in respective opposite senses, and wherein said first and second reflective discs or mirrors are both concave mirrors, arranged with their concave sides facing one another and wherein a wire grid polariser is located between the mirrors
5 inclined at an angle with respect to the two mirrors so as to receive radiation, from a scene being scanned, arriving transversely with respect to said first and second axes and to reflect a plane polarised component of such radiation towards said first mirror, and wherein a quarter wave plate, Faraday rotator or equivalent device is located between said first mirror and said wire grid
10 polariser, whereby the radiation passing to said first mirror and. reflected thereby towards said second mirror has its polarisation direction shifted through 90 degrees in passing twice through said quarter wave plate, Faraday rotator or equivalent device, and can thus pass through said wire grid polariser to said second mirror to be focussed by said second mirror onto a radiation detector or
15 receiver located between said first mirror and said second mirror.

The present invention makes it possible to manufacture a system for providing multiple linear scans, in a compact arrangement that is suitable for use in high-speed mm-wave and microwave applications.

20

Embodiments of the invention are described below with reference to the accompanying schematic drawings in which:-

25

Figure 1 is a perspective view representing part of a first embodiment of the invention,

Figure 2 is a schematic plan view of the part of the apparatus shown in Figure 1,

Figure 3 is a schematic side view of a second part of the apparatus,

Figure 4 is a plan view incorporating a ray diagram illustrating operation of the apparatus of Figures 1 to 3;

Figure 5 is a plan view similar to Figure 4 but illustrating a variant arrangement;

Figure 6 is a plan view similar to Figure 4 but illustrating a yet further variant;

Figure 7 is a schematic side view of part of another apparatus embodying the invention;

Figure 8 is a view similar to Figure 7, incorporating a ray diagram;

Figures 9, 10 and 11 are views similar to Figures 6 and 7 of respective variants,

Figure 12 is a schematic diagram illustrating part of a yet further variant; and

Figure 13 is a sectional view illustrating a practical arrangement embodying the operational principle to which Figure 12 relates.

Referring to Figure 1, a millimetre wave scanning apparatus comprises a hollow polygonal drum 10 which is mounted in a supporting structure (not shown) for rotation about an axis A passing through the centre of the drum. For the purposes of the following description, it is assumed that the drum 10 comprises preferably an even number of side panels extending vertically, i.e. parallel with central axis A, the configuration of the drum being such that in cross-section perpendicular to the axis A, the side walls or panels define a figure which is a regular polygon with an even number of sides, except that, as indicated below, each side wall of the drum is actually made slightly concave on its interior side. The faces or sides of the drum are constructed as wire grid polarisers and thus each may comprise an array of parallel conductors or wires,

for example supported mechanically by a supporting means (not shown) transparent to the radiation concerned. In each face or side of the drum, the parallel conductors or wires extend at 45° with respect to the direction of the axis A of the drum, the sides of the drum being identical with one another so that, as viewed in Figure 1, the parallel wires or conductors of the drum side wall nearest the observer, and lying between the observer and the axis A, extend from top left to bottom right, whilst the parallel wires or conductors of the diametrically opposed side of the drum, and lying beyond the axis A from the point of view of the observer, extend from top right to bottom left. Accordingly radiation passing from the position of the observer in Figure 1, through the side wall of the drum nearest the observer will be plane polarised in one direction at 45° with respect to the direction of the axis A, that direction being such that such polarised radiation will be reflected back towards the observer, (and thus towards the axis A), from the side wall of the drum which is furthest from the observer in Figure 1.

As noted above, the sides of the drum, or at least the notional surfaces on which lie the wires of the wire grid polarisers, are not precisely planar, but are slightly concave on their sides facing towards the axis A, and are configured so as to form concave mirrors, so that, for example, as illustrated in Figure 2, a parallel beam of radiation 11 passing through one side 12 of the drum from the outside, along a diameter of the drum, in a direction parallel with the principal optical axis of the drum side 14 from which it is to be reflected, will be focussed by side 14 towards a focal point which may be substantially on the axis A, as illustrated in Figure 2.

Thus, referring to Figures 1 and 2, the face 14 acts as a concave mirror and focuses the incident radiation, normal to face 12, onto the axis of rotation A

of the drum B. As the drum rotates, so rotation from different azimuthal angles is brought to a focus at the axis A of rotation.

Referring to Figure 3, a rotating reflective member 16 is mounted within
5 the drum for rotation about the axis A, (or about a parallel axis). This second rotating reflector 16 is also mounted in stationary supporting structure (not shown) for such rotation and means (not shown) is provided for rotating the member 16 about its axis, at one half the speed of the primary drum 10 and in the same rotational sense. The rotating reflective member 16 comprises a
10 plurality of radiation reflective faces or facets and has, in cross-section perpendicular to its rotary axis, the form of a regular polygon centred on that axis, with the number of sides being twice the number of sides of the drum 10, said sides being defined by said faces or facets. The reflective member 16 may simply comprise a plurality of generally vertical substantially flat reflective
15 sides parallel with the rotary axis of the member 16, and may be arranged to reflect radiation directly onto a receiver array (not shown) within the primary drum 10. However, for reasons explained below, it is preferred that the reflective member is of the "waisted" form shown in Figure 3.

20 It will be appreciated that radiation passing from outside the primary drum 10 from the scene being scanned, substantially normal to the primary drum side wall which is for the time being the entry side for such radiation, can be regarded as a beam of radiation from the scene scanned and which sweeps around the axis A as the drum 10 rotates. This beam, after reflection at the
25 rotating secondary reflector/reflective member 16, is substantially stationary, allowing it to be collected effectively by a stationary radiation detector (not shown), which may be mounted within the drum 10. Thus, as the drum 10 rotates, one of its faces at a time is used to scan the scene. At the limit of the scan the radiation being collected by the radiation detector from the scene

scanned passes from one face of the secondary reflective member 16 to the next and the next face of the rotating drum 10 becomes that through which the radiation reaching the radiation detector from the scene scanned passes and thus the next scan begins.

5

The location of the stationary radiation detector or detector array is in general a matter to be determined by considerations of mechanical convenience, requirements for compactness, etc. However it is possible to take advantage of the polarisation of the radiation after reflection by the reflective member 16 to
10 minimise radiation losses between reflective member 16 and the radiation detector array. For example, it may be convenient to locate the radiation detector or detector array outside the drum 10 and to reflect the radiation from the reflective member 16 through the side walls of the drum 10 to the radiation detector or detector array. In this case, it is generally necessary to ensure that
15 direction of polarisation of the radiation after reflection from reflective member 16 towards the radiation detector or detector array is rotated through 90 degrees (with respect to its direction of polarisation before striking the secondary reflective member), before the radiation reaches the side walls of drum 10 in order to allow the radiation to pass through such side walls. This may be done
20 by placing a Faraday rotator or a quarter wave plate within the drum in front of reflective member 16 and between reflective member 16 and the radiation detector or detector array. Alternatively, as illustrated in Fig. 3, the central reflective member 16 may be of the waisted form shown, comprising a plurality of pairs of reflective facets, the facets of each pair being perpendicular or
25 nearly perpendicular to each other, equally and oppositely inclined with respect to the rotational axis of the central drum and so disposed that the line of intersection of the facets of each said pair forms a respective side of a regular polygon centred on the rotational axis of the member 16 said polygon, (as noted above) having twice the number of sides as the main drum 10. Again, of

course, the central secondary reflector 16 rotates at half the speed of the main drum 10. As illustrated, incoming radiation 17 strikes, e.g. an upper facet 19 of the member 16, is reflected by upper facet 19 onto the lower facet 21 of the respective pair of facets and is reflected from that lower facet back away from the member 16. The radiation is thus reflected twice by the member 16 and is thus reflected from the secondary reflector 16 with the correct polarisation to pass through the outer drum 10.

In the arrangement shown in Figure 4, after reflection at the central reflective member 16, represented by centre point 16 in Figure 4, the radiation, having had its direction of polarisation rotated through 90 degrees by any of the expedients discussed above, passes through the main drum and is focused onto a vertical array 26 of radiation detectors (assuming the rotary axis A of the drum 10 to be vertical). In the arrangement illustrated in Figure 4, radiation directed from the drum 10 by the secondary reflector 16 is reflected by a concave mirror M1 onto the detector array 26, which in the arrangement shown is located within the drum 10. However, the mirror M1 may be arranged instead to direct the radiation onto a receiver array outside the drum 10 or may be dispensed with and the side walls of drum 10 configured so that the radiation, after reflection by secondary reflector 16, comes to a focus on a receiver or receiver array within or outside the drum.

In another variant, illustrated in Figure 5, a concave mirror M1 outside the drum 10 again reflects radiation passing from the drum 10 back into the drum 10 but in this variant a further mirror M2, (which may also be a concave mirror), within the drum 10, is provided which in turn reflects the radiation onto a stationary vertical receiver array 28 outside the drum. In this variant, in order that the mirror M2 does not obstruct the field of view, the mirror M2, like the side walls of drum 10, is configured so that it reflects radiation with one

direction of polarisation and transmits radiation with the orthogonal direction of polarisation. In a further variant, illustrated in Figure 6, both the mirror M1 and the mirror M2 are located within the drum 10 and each is configured so that it reflects radiation with one direction of polarisation and transmits radiation with the orthogonal direction of polarisation, so that the mirrors M1 and M2 do not obstruct the field of view.

Assuming the central axis A to be vertical, the features of the arrangements thus far described only provide a horizontal scan of the field of view. If, as is generally required, a two-dimensional field of view is required, a raster type scan in which the horizontal scan provides a line scan may be provided by any of the expedients described for this purpose in WO03/012524. As an example, a line scan may be provided by providing a vertical array of radiation detectors, so that the number of raster lines would equal the number of detectors in the array. Alternatively, the side walls of drum 10, instead of being strictly vertical, i.e. parallel with the axis A, (or rather instead of having their principal axes extending strictly radially with respect to the axis A), may be variously inclined slightly to the axis A so that successive faces of the drum 10 would cause a different horizontal scan line in the field of view to be focused on a single receiving element. By combining these possibilities it is possible to obtain a scanning raster in which the number of scan lines is equal to the product of the number of receivers in a vertical receiver array by the number of faces of the drum 10. Thus, if the drum 10 has six faces, as illustrated, the number of horizontal scan lines in the scanning raster will be six times the number of receivers in the array.

As a further possibility, in arrangements corresponding to those illustrated in Figure 4, 5 or 6, one or possibly both of the mirrors, M1 and M2 could be arranged to tilt about an axis perpendicular to the axis of rotation of the hollow

drum 10, so as to effect a "field scan" as the rotating drum 10 produces a line scan.

In a further variant, the secondary reflective member 16 could be
 5 configured as a prism having roof reflectors and the orthogonal or field scan could be achieved by displacing this prism along its axis of rotation. Either the whole prism could be displaced as a function of time or else this prism could be fixed and individual reflectors displaced with respect to their neighbouring reflectors as a function of time.

10

Figures 7 to 12 illustrate alternative embodiments of scanning apparatus for producing a linear scan pattern, in accordance with the second aspect of the invention. In these embodiments, the scanning arrangement consists of two counter-rotating radiation reflective discs which are mounted for rotation in
 15 supporting structure (not shown) about respective axis. The planes of the discs are tilted slightly with respect to their axes of rotation, i.e. so that the normal to the plane of each disc is inclined slightly with respect to its rotational axis.

In the arrangement of Figure 7, these discs are plane mirrors, 50, 52 and the
 20 normals to the planes of the mirrors are tilted by the same angle with respect to the respective axes of rotation 50A, 52A of the discs 50, 52. The mirrors 50, 52 rotate at the same rate as each other but in opposite senses.

In the arrangement shown in Figure 7, the axis 50A, 52A are coincident, i.e.
 25 they are one and the same, but this is not essential. A fixed wire grid polariser 54 is mounted between mirrors 50, 52 at about 45° to the axis of rotation of the two mirrors, 50, 52. Ideally, the transmission axis of the polariser 54 should be parallel with or perpendicular to the plane of incidence of the radiation arising from the centre of the field of view of the scanner. Plane polarised radiation

from the scene being scanned is reflected from the polariser 54 onto the first rotating mirror 50, after passing through a component 56 which may be a quarter wave plate or alternatively a Faraday rotator. The radiation reflected by the first rotating mirror 50 passes back through the quarter wave plate, (or Faraday rotator) 56, after which its direction of polarisation has been rotated by 90° with respect to the radiation reflected towards mirror 50 from the wire grid polariser 54. In this case, the radiation reflected at the first rotating mirror 50 passes through the inclined polariser 54 and falls on the second rotating mirror 52, after passing through a second component 58 which again is a quarter wave plate or Faraday rotator.

On reflection at the second rotating mirror 52, this radiation passes back through the second quarter wave plate or Faraday rotator 58 and is reflected at the inclined polariser 54 as illustrated by the ray diagram in Figure 8.

When the radiation is thus reflected for the second time by the plane polariser 54, it leaves the linear scanner arrangement shown (leaving towards the right in Figure 8 in substantially the same direction as the incoming radiation from the scene being scanned), and passes either to an orthogonal linear scanner, (to effect a frame scan of a scanning raster whilst the rotating discs provide the line scan of the raster), or to a linear array of radiation detectors as discussed above and as disclosed in WO03/012524. The direction of line scan depends on the phase of the two counter-rotating inclined mirrors 50,52. For example, if the two mirrors are parallel when viewing the middle of the field of view, then the scan direction is substantially horizontal, assuming that their axes of rotation 50A, 52A are vertical.

In other embodiments, any one or both of the rotating mirrors may be curved. For example, the first rotating mirror 50 may be slightly curved to correct for

spherical aberrations and may additionally be concave to provide a converging effect on radiation reflected towards the second rotating mirror, whereby the size of the second rotating mirror may be reduced. It is not possible to reflect from a powered mirror at a significant off-axis angle without introducing
5 --- serious aberrations. However, the use of the polarising beam splitter 54 inclined at 45° with respect to the rotary axis of discs 50, 52, between the two rotating discs, makes it possible to achieve a near-normal incidence and reflection of radiation at the first rotating mirror 50. The second mirror 53, in this arrangement, may, as shown in Figure 9, be sufficiently spherically
10 --- concave to produce a real image of the scene scanned close to the polarising fold mirror 54 as illustrated in Figure 9.

In the scanning arrangement illustrated in Figure 9, if the second quarter wave plate, (or Faraday rotator) 58 is omitted, then, as illustrated in figure 10, the
15 --- radiation reflected at the second rotating mirror 52 passes back through the inclined polariser 54, to be reflected again from mirror 50, to strike polariser 54 again and be reflected by the polariser to form an image on the input side of the scanner. A detector, or an array of detectors, may be placed at this image surface.

20 --- In this optical arrangement, the first rotating mirror is reflected from twice and its inclination must be half the effective inclination of the second rotating mirror. An advantage of this latter configuration is that pupil wander in a direction parallel to the direction of scan is effectively removed.

25 --- The scanning mechanisms illustrated in Figures 9 and 10 may be used to produce a two dimensional image of the scene by placing a linear array of detectors at the focal plane. The direction in which the line of detectors in this detector array extends is perpendicular to the direction of line scan.

Alternatively, the radiation leaving this scanning mechanism may pass to a separate orthogonal scanner. The orthogonal (frame) scan may also be achieved by tilting the plane polariser 54 in Figures 9 and 10 respectively back and forth about an axis of rotation through its centre. Thus, the rotating discs

5 50, 52 could be used to produce a (line) scan of the scene in a direction perpendicular to their axis of rotation, while the plane polariser 54 could be tilted about an axis in the same direction as the scan. In this way, a two dimensional scanning raster may be generated. This is illustrated in Figure 11. Radiation from the scene scanned is reflected from the polariser 54 which may

10 be tilted about a horizontal axis. This reflected radiation falls on to the first rotating mirror 50 after passing through the Faraday rotator (or quarter wave plate) 56. On reflection at the first rotating mirror 50, the radiation passes again through the Faraday rotator (or quarter wave plate) 56 with its direction of polarisation now at 90° to that of the radiation originally reflected from the

15 polariser 54. This radiation is therefore able to pass through the polariser 54 and be incident at the second rotating mirror 52. On reflection at the second rotating mirror, the radiation again passes through the polariser 54 and falls on the first rotating mirror 50 for a second time. When it is reflected now by mirror 50, the radiation passes to a single element receiver or multi-element

20 array located at the point F in Figure 11. It may be necessary to cut a hole in the polarising plane mirror 54 and to use a plane fold mirror located near the centre of mirror 54 to reduce obscuration (this would place the focal point and the position of the receiver to the right of the structure in Figure 11. Motion of the polarising mirror 54 about its horizontal axis causes a vertical scan of the

25 scene. The two rotating mirrors 50, 52 are, as in the embodiments of Figure 7 to 10, tilted about their axis or axes of rotation and rotate at the same speed as one another but in opposite directions.

With an appropriate initial relative phase in their rotational positions, the rotating discs 50, 52, may perform a horizontal (line) scan of the scene scanned. The effective tilt on the second rotating mirror 52 on its axis is ideally twice that of the first 50 on its axis. For a plane mirror 52, this effective tilt is equal to its actual tilt but for a powered second rotating mirror, the actual tilt is equal to the effective tilt multiplied by a factor of $(1 - x/R)$ where x is the spacing between the two rotating mirrors and R is the radius of curvature of the powered mirror. In this context, a concave mirror has a positive value of R . For a powered, e.g. convex, mirror, the actual tilt is, of course, the angle between the principal axis, (axis of symmetry) and the rotational axis.

In yet another embodiment, the first and second rotating tilted mirrors perform both the high speed line scan pattern and the orthogonal (frame) scan. In this case, each mirror rotates about two axes. Thus, referring to Figure 12, in this arrangement, for each mirror, its rotational axis B is arranged to precess about another axis A. In this example, the normal through the centre of each mirror is tilted at an angle β to the local axis of rotation B of the mirror and this axis B itself rotates, at a slower speed, about a fixed axis A and makes an angle α to the axis A. Each mirror rotates at the same high speed about its respective local axis B and in combination performs a substantially linear (line) scan pattern of the scene. The two axes B also rotate at the same slower speed as one another about their respective axes A, to produce an orthogonal (field) scan. The relative angles of inclination α and β on each rotating mirror and the direction and phase relationships between the rotating mirrors 50 - 52 are such that the two mirrors perform a raster scan of the scene. In the last noted system, the optical arrangement (ignoring the precession of the rotational axes of the mirrors 50, 52), is as illustrated in Figure 11, the wire grid polariser 54 in this case being fixed whilst the two mirrors 50 - 52 rotate and precess in opposite

directions when viewed along the axis A of precession of one of the mirrors.

When the axes of precession are vertical, then a substantially horizontal line scan may be achieved of the scene with the high speed rotation and a vertical frame scan may be achieved with the lower speed angular precession. Since, as
 5 in Figure 11, two reflections occur at the first rotating mirror, (corresponding to mirror 50) and only one reflection at the second mirror (corresponding to mirror 52), the effective angle β of inclination and α of inclination of the rotational axis with respect to the precession axis, for the first mirror, are half of those for the second mirror.

10

The actual angles of inclination (β) and precession α depend on the desired fields of view and curvatures of each rotating mirror. For example, if the first mirror were substantially plane, then a tilt of 2.5° of this mirror and an effective tilt of 5° of the second mirror would achieve a horizontal line scan of plus or
 15 minus 20° . Similarly an angle of precession of 2.5° on the first mirror and an effective angle of precession of 5° on the second mirror could achieve a vertical frame scan also of plus or minus 20° .

The actual angles of tilt and procession on the second mirror are the effective
 20 values multiplied by $(1 - x/R)$ where x is the spacing between the upper and lower mirrors and where R is the radius of curvature of the second (lower) mirror in Figure 11.

The frame rate and number of scan lines in the scan pattern depends on the
 25 actual speeds of the high-speed rotation and the lower speed procession. There are two scan lines per rotation and two frames per procession. So to achieve a frame rate of 10Hz the procession speed is 300rpm. Also with 100 scan lines per frame and 10 parallel receiver channels the speed of rotation is 3000rpm.

In this situation the actual number of useable scan lines is less than 100 since the scan lines overlap towards the top and bottom of the frame.

5

The high speed rotation and lower speed precession of the arrangement described above may be achieved, for each mirror using the mechanical arrangement shown in Figure 13 in which a high speed rotating shaft 70 rotates the mirror 50', 52' - via a universal joint 72, (preferably a constant velocity universal joint). The shaft 70 is journalled in a sleeve 74 and a bearing portion 10 76 fixed to or integral with the sleeve 74 carries bearings in which a shaft 78 carrying a mirror mount 80 is supported for rotation, the universal joint referred to connecting the shaft 78 with the shaft 70. The rotational axis of shaft 78 corresponds with the axis B in Figure 12 whilst the rotational axis of the shaft 15 70 corresponds with the axis A in Figure 12. In the arrangement shown in Figure 13, the mirror mount 80 is shown as comprising a plate arranged perpendicular to the axis of shaft 70 and a wedge 82, having a wedge angle β , is interposed between the mirror 50, 52 and the aforesaid perpendicular plate. It will be appreciated, of course, that in a production version, the wedge 82 and 20 plate 80 may be formed as an integral component. The sleeve 74 is in turn supported by bearings 84 for rotation in a stationary supporting structure, indicated only fragmentarily at 86 in Figure 13.

In Figure 13, reference 88 represents a plate fixed to one end of the sleeve 74 25 perpendicular to the axis of the latter and the frame part 76 is shown as having the general form of a plate generally perpendicular to the axis of the shaft 78. Thus the angle α between the faces of the last-noted plate and the plate 88 is the angle α of the arrangement of Figure 12. It will be appreciated, of course, that

the components 76, 88, 74 may, as indicated above, be formed as an integral structure and need not have the specific form shown provided that the angle α between the axis of shaft 78 and the axis of shaft 70 is maintained. Means, not shown, is provided for rotating the shaft 70 at an appropriate relatively high speed and for rotating the sleeve 74 at the appropriate lower speed of precession.

- There has been described above the addition of a precession to the rotational axis of the mirror discs of the rotating disc scanner illustrated in Figure 11.
- 10 This principle may also be applied to other forms of two-rotating-tilted-mirror scanners to achieve a two dimensional (raster) scan pattern. The same principal may also be applied to single-tilted-rotating-mirror scanners to achieve an improved utilisation of receiver channels.
- 15 In addition, the provision for precession of the rotational axis may also be applied to rotating polygon scanners such as that described with reference to Figures 1 to 4, to achieve a two dimensional scan pattern from an otherwise one dimensional scanner, for example by arranging the rotational axis (corresponding to axis B Figure 12) of the rotating polygon or drum at a tilt
- 20 angle, (corresponding to angle (α) in Figure 12) with respect to an axis (corresponding to axis A in Figure 12) with respect to an axis (corresponding to axis A in Figure 12) of precession, about which the spin axis (corresponding to axis B) is arranged to precess at a slower rate than the rate of spin about the spin axis.

CLAIMS

1. A scanning apparatus operable in the microwave, mm-wave, sub
5 mm-wave and infrared ranges and comprising a support structure, a primary
drum which is mounted in said support structure for rotation relative to the
support structure about a central axis of the primary drum, said primary drum
being hollow and of rectangular polygonal form to provide a number of sides or
facets each adapted to transmit such radiation which is plane polarised in a first
10 direction at 45° with respect to the rotary axis of the drum and to reflect
radiation which is plane polarised in a direction at 45° to the rotary axis of the
drum and perpendicular to the said first polarisation direction, such radiation
emanating from a field of view of the apparatus, being a field of view which is
fixed with respect to said supporting structure, (as opposed to rotating with the
15 primary drum), the arrangement being such that radiation passing into the drum
through whichever said side of the drum is currently facing said field of view
and passing towards the diametrically opposite side will be plane polarised with
a polarisation direction such as to be reflected back by said diametrically
opposite side towards the rotary axis of the drum, each said polygon side being
20 configured so as to act, when reflecting such radiation striking that side from
within the drum, as a concave mirror, to focus the radiation towards a receiver
assembly which includes a radiation detector for such radiation.

2. Apparatus according to Claim 1 in which said radiation detector is
25 stationary with respect to said support structure and said receiver assembly
includes means whereby the radiation reflected from such diametrically
opposite side of the rotating drum reaches said radiation detector as a
substantially stationary cone.

3. Apparatus according to Claim 1 in which said receiver assembly includes a radiation reflective member mounted within the primary drum for rotation, in said support structure, about an axis coincidental with or parallel with said central axis of the primary drum, the apparatus including means for rotating said radiation reflective member at one half the speed of the primary drum, and in the same rotational sense, said radiation reflector having a plurality of radiation reflective facets and being such that, in section in a plane perpendicular to its rotary axis said reflective facets define a regular polygon with twice as many sides as the primary drum, said receiver assembly further including means for receiving radiation reflected from said radiation reflective member, and for directing radiation so received to said radiation detector.

4. Apparatus according to Claim 3 wherein said means for receiving radiation reflected from said radiation reflective member is located outside the primary drum and wherein said radiation reflective member is arranged to reflect such radiation, to said means for receiving, through the sides of the primary drum, means being provided within the drum and interposed between said radiation reflective member and said means for receiving for rotating the polarisation direction of such radiation through 90° to pass through said sides of the primary drum.

5. Apparatus according to Claim 3 wherein said radiation reflective member comprises a plurality of pairs of reflective facets, one facet of each pair being disposed further along said axis of the reflective member than the other, the number of such pairs being twice the number of facets of the primary drum, and wherein the facets of each pair are so arranged that radiation directed onto one of said facets after reflection from a said side of the primary drum will be

reflected onto the other facet of the pair to be reflected thereby through the sides of the primary drum, to said means for receiving.

6. Apparatus according to Claim 5, wherein the two facets of each
5 said pair are perpendicular to one another.

7. Apparatus according to Claim 6 wherein the two facets of each
said pair are inclined at opposite 45° angles to the rotary axis of said radiation
reflective member.

10

8. Apparatus according to Claim 3 wherein said means for receiving
radiation comprises an element, herein referred to as a transreflector, mounted
within the primary drum and arranged not to obstruct plane polarised radiation
reflected from a said facet of the primary drum towards said radiation reflective
15 member but to reflect directly or indirectly to said radiation sensing means,
radiation reflected onto said transreflector by said radiation reflective member.

9. Scanning apparatus operable in the microwave, mm-wave and
infrared ranges and comprising a support structure, a first reflective disc or
20 mirror which is mounted in said support structure for rotation relative to the
support structure about a first axis, a second reflective disc or mirror which is
mounted in said support structure for rotation relative to the support structure
about a second axis, the arrangement being such that radiation from a scene
being scanned can reach a reflective surface of the first disc or mirror to be
25 reflected thereby onto a reflective surface of the second disc or mirror, to be
reflected by the latter, in turn, onto a further part of the apparatus incorporating
a receiver or receivers for such radiation, and wherein said reflective surface of
the first disc or mirror has an axis of rotational symmetry, (or a normal where
said surface is planar), tilted at a small angle relative to said first axis and

wherein said reflective surface of the second disc or mirror has an axis of rotational symmetry (or a normal where said surface is planar) tilted at a small angle relative to said second axis, and driving means for said discs or mirrors arranged to drive these in respective opposite senses, and wherein said first and
5 second reflective discs or mirrors are both concave mirrors, arranged with their concave sides facing one another and wherein a wire grid polariser is located between the mirrors inclined at an angle with respect to the two mirrors so as to receive radiation, from a scene being scanned, arriving transversely with respect to said first and second axes and to reflect a plane polarised component
10 of such radiation towards said first mirror, and wherein a quarter wave plate, Faraday rotator or equivalent device is located between said first mirror and said wire grid polariser, whereby the radiation passing to said first mirror and reflected thereby towards said second mirror has its polarisation direction shifted through 90 degrees in passing twice through said quarter wave plate,
15 Faraday rotator or equivalent device, and can thus pass through said wire grid polariser to said second mirror to be focussed by said second mirror onto a radiation detector or receiver located between said first mirror and said second mirror.

20

10. Apparatus according to Claim 9 wherein a further Faraday rotator or quarter wave plate or equivalent device is located between said wire grid polariser and said second mirror, whereby radiation passing through said second mirror and reflected thereby towards said first mirror has its polarisation
25 shifted through 90° in passing twice through said second quarter wave plate, Faraday rotator or equivalent device and is reflected by said wire grid polariser, in a direction away from the scene being scanned, towards a radiation detector or receiver.

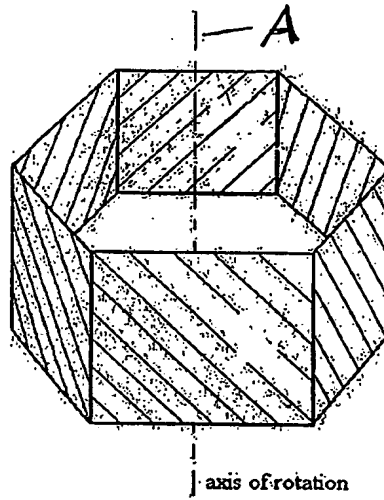
11. Apparatus according to Claim 10 wherein said second mirror is arranged to direct said radiation to said radiation detector or receiver indirectly, by directing said radiation again through said quarter wave plate, Faraday rotator or
5 equivalent device to said first mirror, to be reflected again, in turn, by said first mirror.

12. Apparatus according to Claim 11 arranged so that after the second reflection by said first mirror and the subsequent passage through the
10 first quarter wave plate, Faraday rotator or equivalent device, the radiation is reflected again by said wire grid polariser, towards said radiation detector or receiver.

13. A scanning apparatus operable in the microwave, millimetre wave, sub
15 millimetre-wave and infrared ranges and comprising at least one scanner mounted for rotation relative to a first support structure about a first axis, to effect a scan of a scene being scanned in one direction and in which said first support structure is itself mounted for rotation with respect to a second support structure, about an axis inclined with respect to said first
20 axis, to effect a scan of the scene being scanned in the orthogonal direction.

14. Apparatus substantially hereinbefore described with reference to and as shown in any one of the accompanying drawings.

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← 10

Fig 1

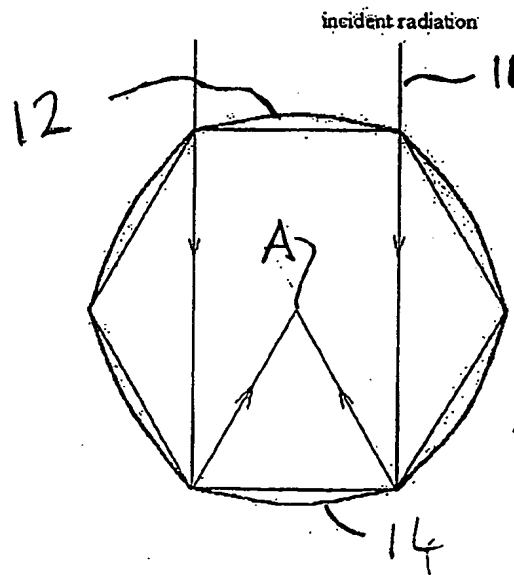


Fig 2

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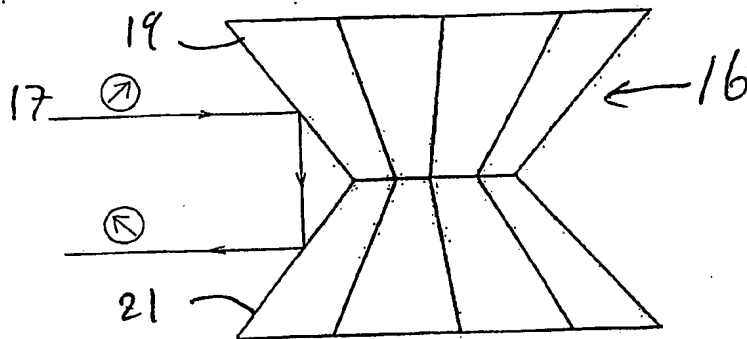


Fig. 3

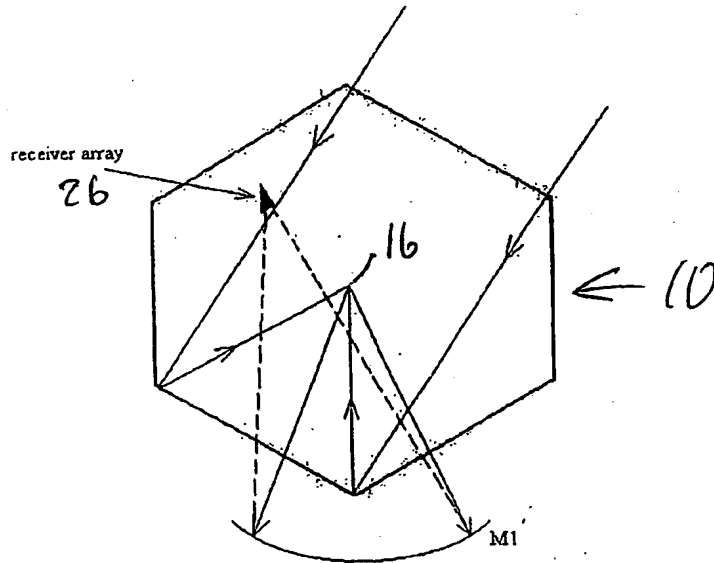


Fig 4

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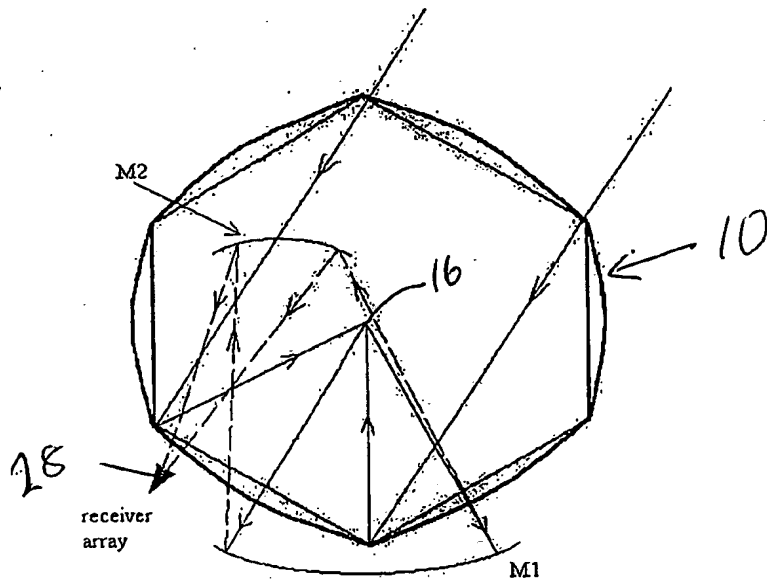


Fig 5

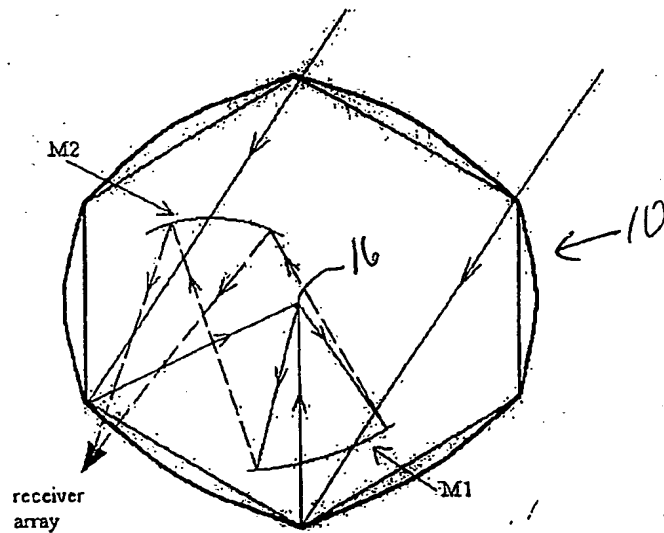


Fig 6

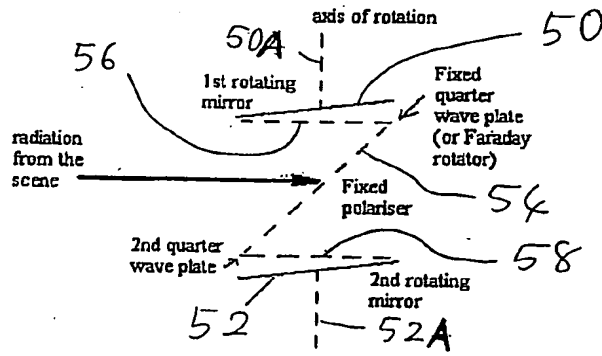


Figure 7

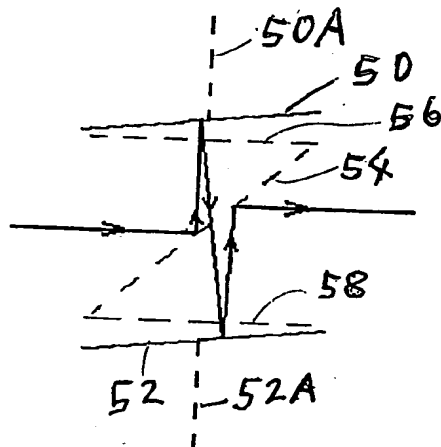


Fig. 8

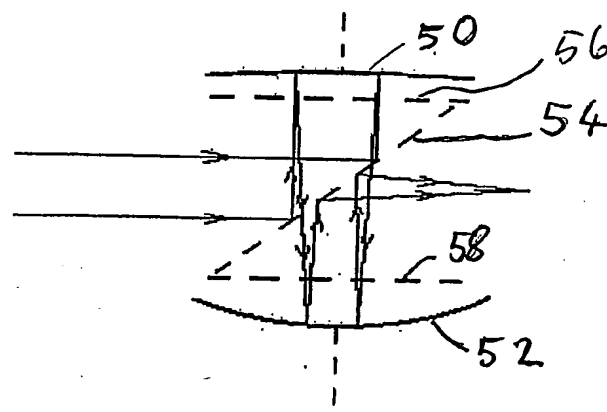


Figure 9

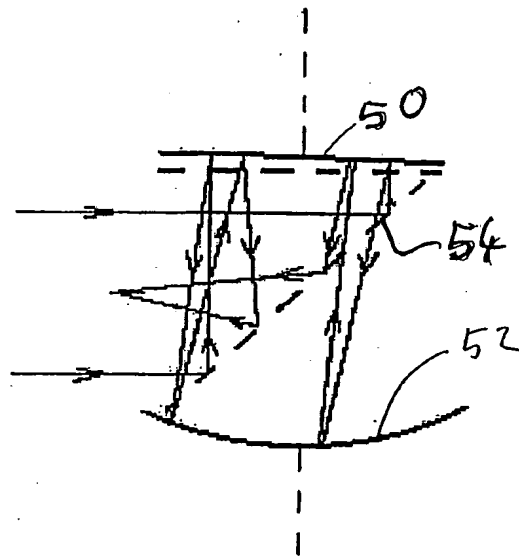


Figure 10

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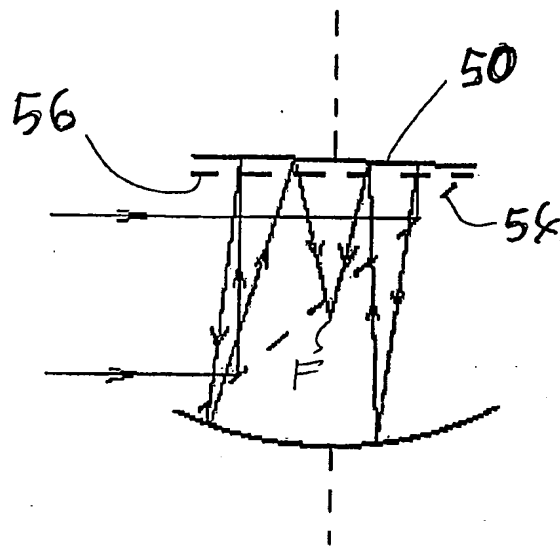


Fig. 11

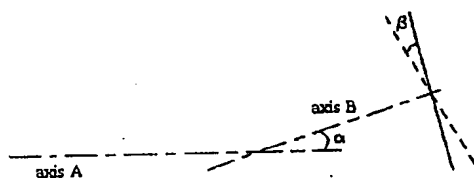


Fig. 12

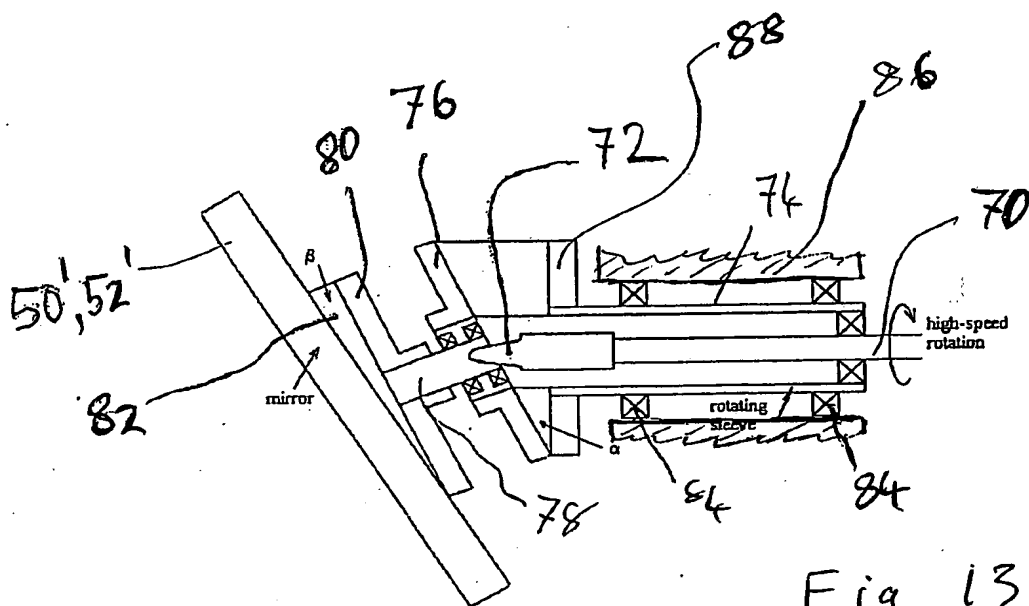


Fig. 13